



THE EFFECT OF INTERPHASE (AUSTENITE/FERRITE) AND INTERGRANULAR BOUNDARIES ON HYDROGEN EMBRITTLEMENT OF A HIGH-NITROGEN AUSTENITIC STEEL

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Outline

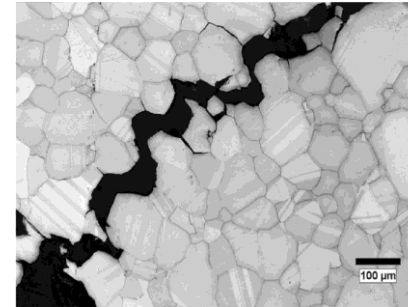


- Motivation
- Materials and methods
- Results:
 - Microstructure characterization
 - Mechanical properties of steel before and after hydrogen-charging.
 - Fractographic analysis
- Summary

Motivation



- **Hydrogen embrittlement**(HE), also known as **hydrogen assisted cracking** (HAC) and **hydrogen-induced cracking** (HIC) was discovered by Johnson in **1875**.



*Hydrogen-Induced Cracks (HIC)**

Diffusible hydrogen is harmful to the plasticity of steels



The harmful influence of diffusible hydrogen can be mitigated:



by preventing its entry into steel

or



by rendering it immobile once it penetrates the material

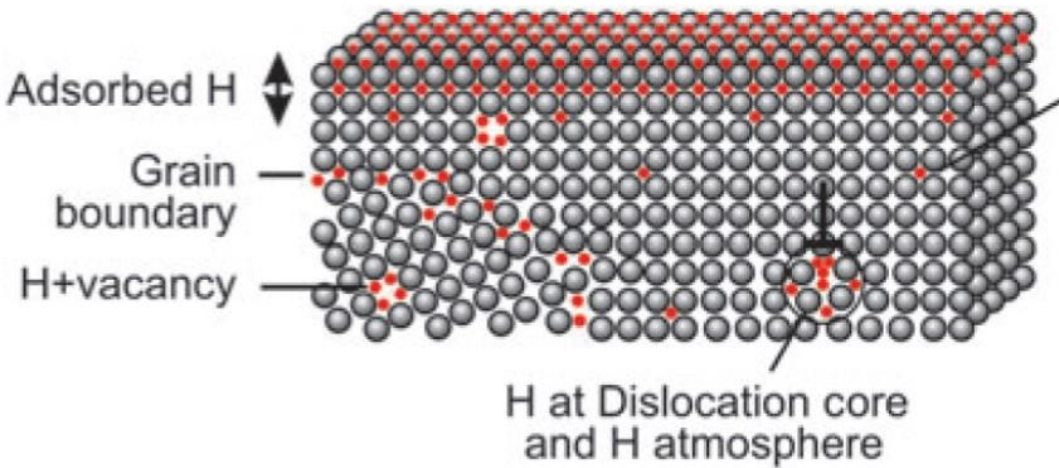
*Iannuzzi, M., Barnoush, A., & Johnsen, R. (2017, April 28). Materials and Corrosion Trends in Offshore and Subsea Oil and Gas Production. <https://doi.org/10.1038/s41529-017-0003>

**<https://seblog.strongtie.com/2015/10/hydrogen-embrittlement-in-high-strength-steels>

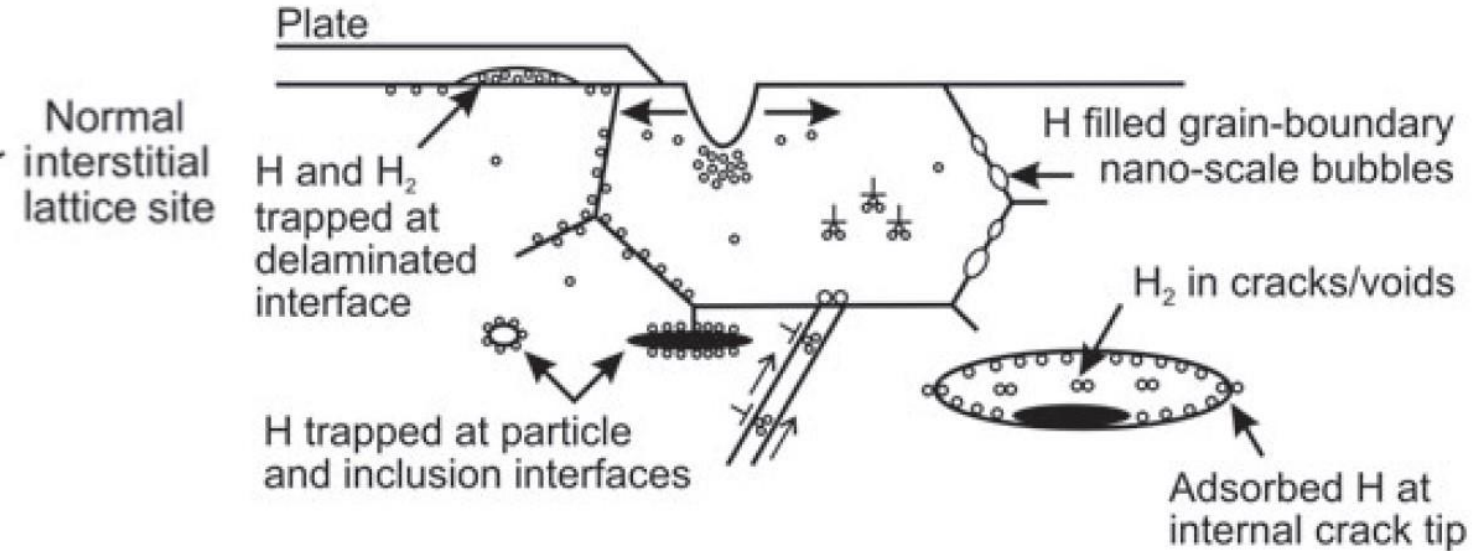
Sites and traps for hydrogen



(a) - on an atomic scale



(b) - on a microscopic scale*

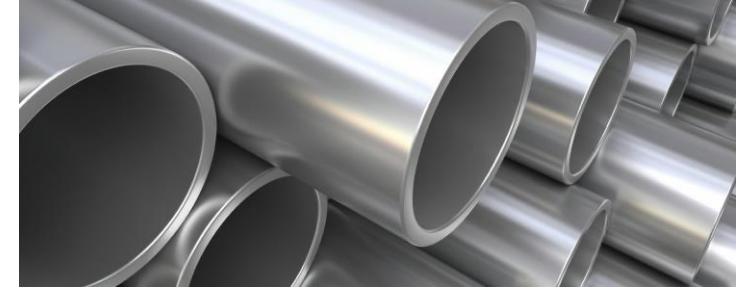


Schematic illustrations of sites and traps for hydrogen in materials

High nitrogen austenitic steels (HNS):



- high strength
- corrosion resistance
- wear resistance



ferrite

High hydrogen diffusivity

Low hydrogen solubility



path to transport hydrogen

austenite

Low hydrogen diffusivity

High hydrogen solubility



sink, trapping hydrogen

THE AIM OF THE RESEARCH

to establish the effect of volume fraction of δ -ferrite and the density of interphase (austenite/ δ -ferrite) and grain (austenite/austenite) boundaries on the mechanical properties and fracture mechanisms of a high-nitrogen austenitic steel before and after hydrogen-charging



- High-nitrogen austenitic steels steel was chosen as an object of the investigation:
Fe-23Cr-17Mn-0.1C-0.6N steel (wt.%) (HNS).

Solid-solution treatments (SST):

- $T_{sst}=1050$ °C, 0,5 h
- $T_{sst}=1100$ °C, 0,5 h
- $T_{sst}=1150$ °C, 0,5 h
- $T_{sst}=1200$ °C, 0,5 h



+H
**Electrochemical
hydrogen-
charging for
100 h**



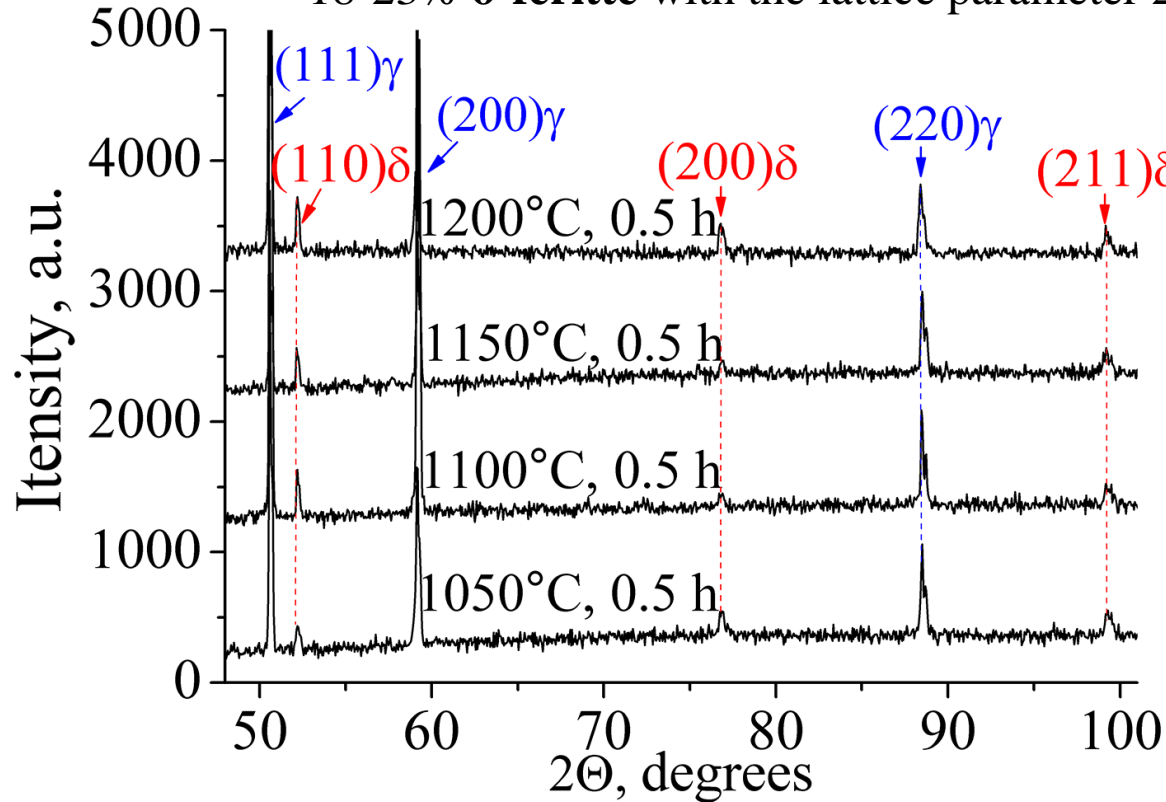
Methods:

- X-ray diffraction (XRD) phase and structural analyses
- Light microscopy (LM)
- Transmission electron microscopy (TEM)
- Tensile tests
- Scanning electron microscope (SEM)

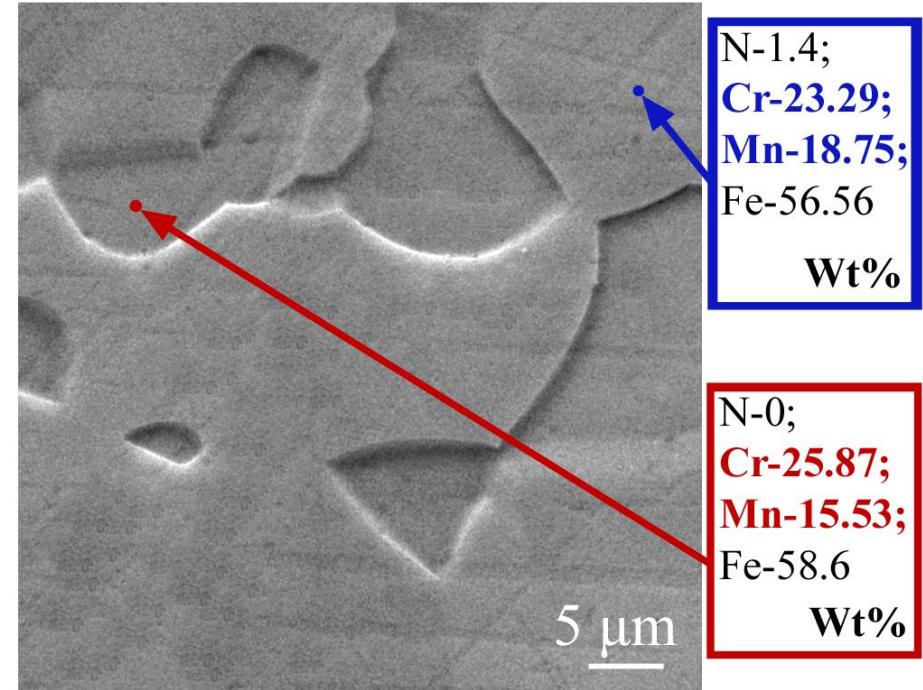
HNS microstructure after different regimes of solid-solution treatment



Austenite (γ -phase) with a lattice parameter $a=3,63 \text{ \AA}$,
18-23% **δ -ferritte** with the lattice parameter $2,88 \text{ \AA}$.



XRD patterns of HNS
solution-treated in
different regimes

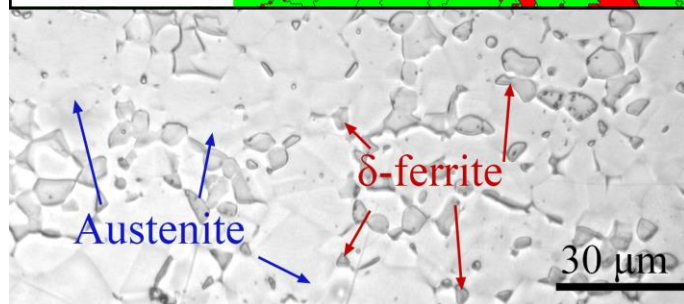
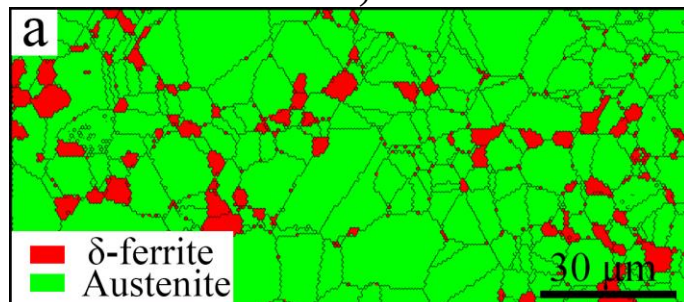


SEM image of a surface of solid-solution treated (1150°C, 0.5 h)
specimen combined with results of Energy-Dispersive X-Ray
Spectroscopy

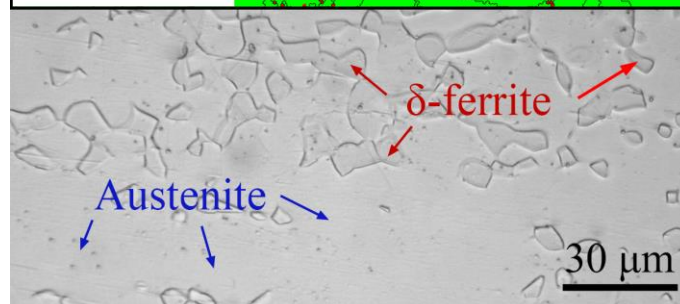
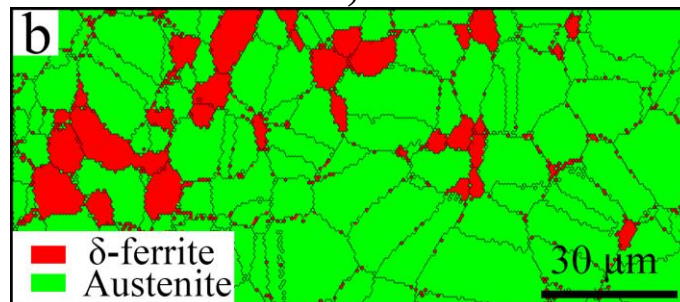
EBSD phase maps and light microscopy images of HNS after different regimes of solid-solution treatment



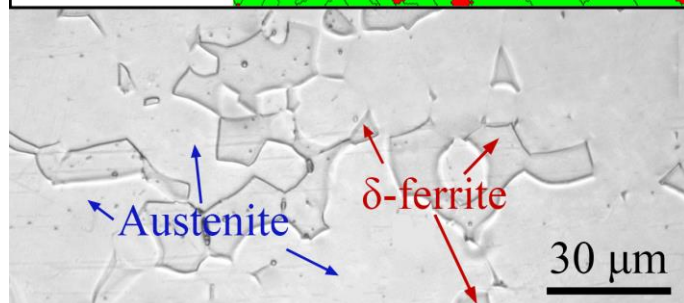
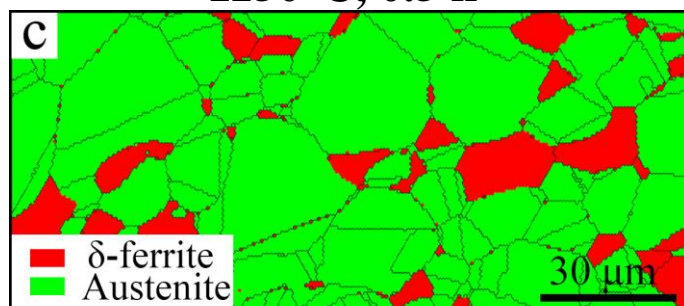
1050°C, 0.5 h



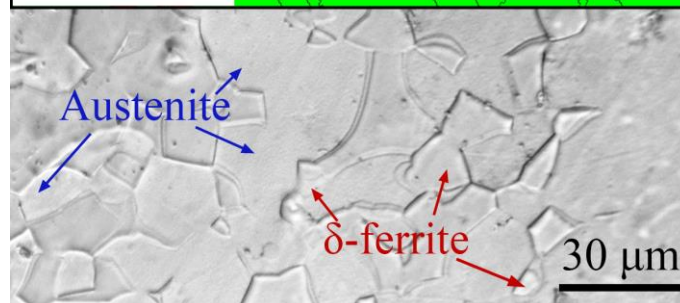
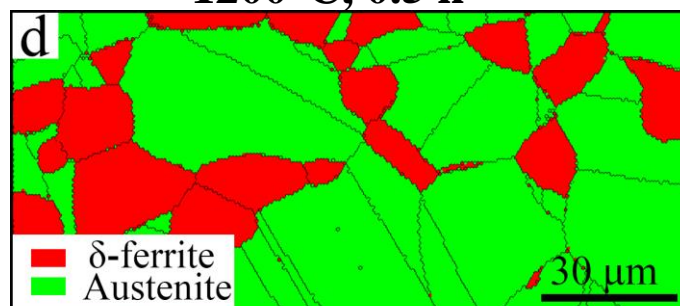
1100°C, 0.5 h



1150°C, 0.5 h

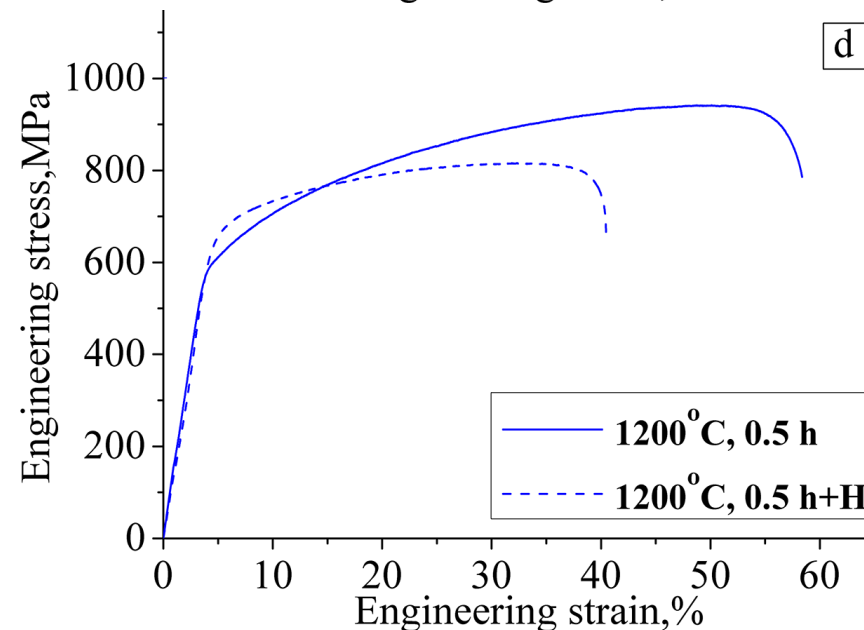
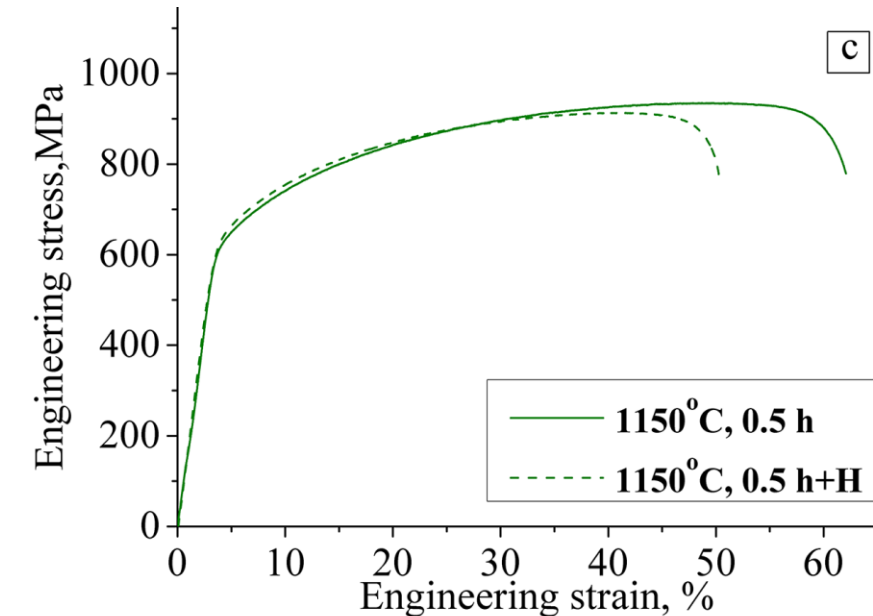
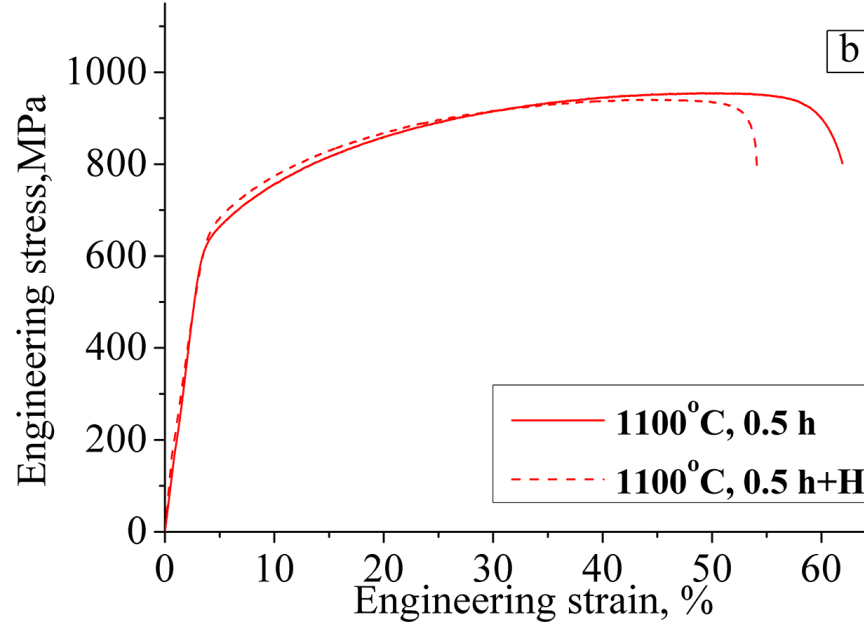
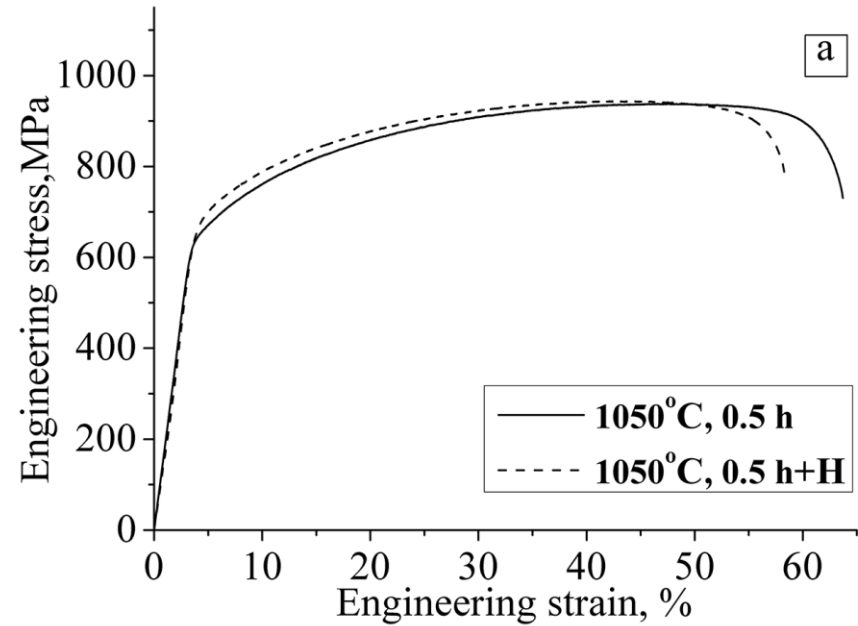


1200°C, 0.5 h



T_{sst}	Average grain size γ -ferrite, μm	Average grain size δ -ferrite, μm	Volume fraction δ -ferrite, %
1050°C, 0.5 h	9.7±5.2	4.9±2.8	18.3
1100°C, 0.5 h	11.7±6.6	6.1±2.5	19.5
1150°C, 0.5 h	16.3±7.9	7.4±4.5	21.3
1200°C, 0.5 h	25.7±13.3	9.5±5.2	23.4

The dependence of mechanical properties of HNS on hydrogen-charging after different regimes of solid-solution treatment



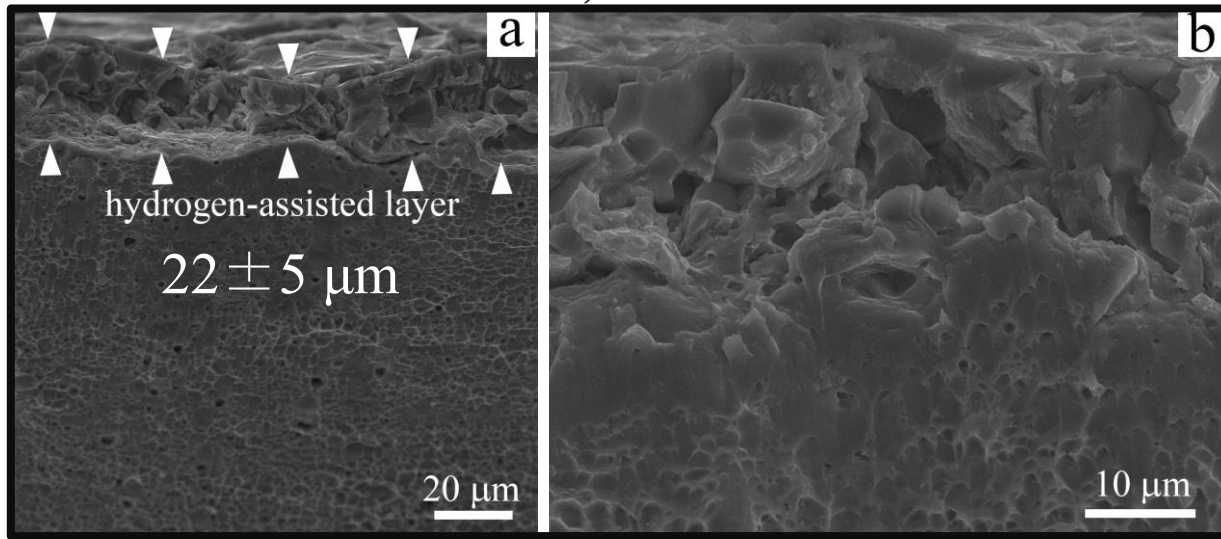
T_{sst}	I_H
1050°C, 0.5 h	10 %
1100°C, 0.5 h	15 %
1150°C, 0.5 h	23 %
1200°C, 0.5 h	32 %

Hydrogen embrittlement index:
 $I_H = [(\delta_0 - \delta_H) / \delta_0] \times 100\%$,

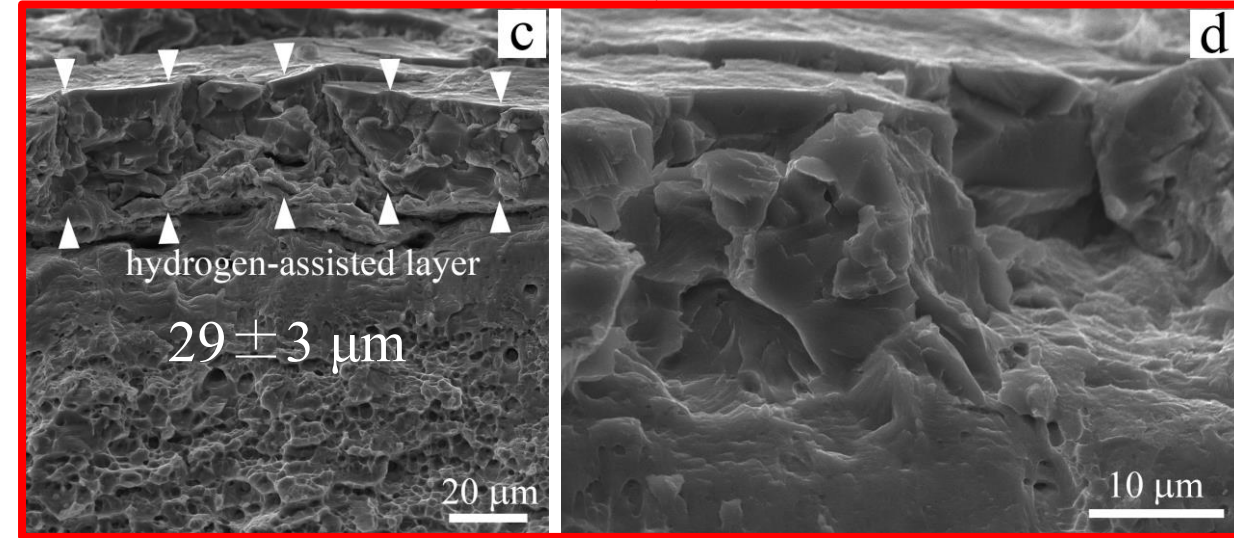
δ_0 and δ_H - total elongation before failure of hydrogen-free and hydrogen-charged specimens, respectively.

SEM micrographs of fracture surfaces in hydrogen-charged specimens of HNS after different regimes of solid-solution treatment

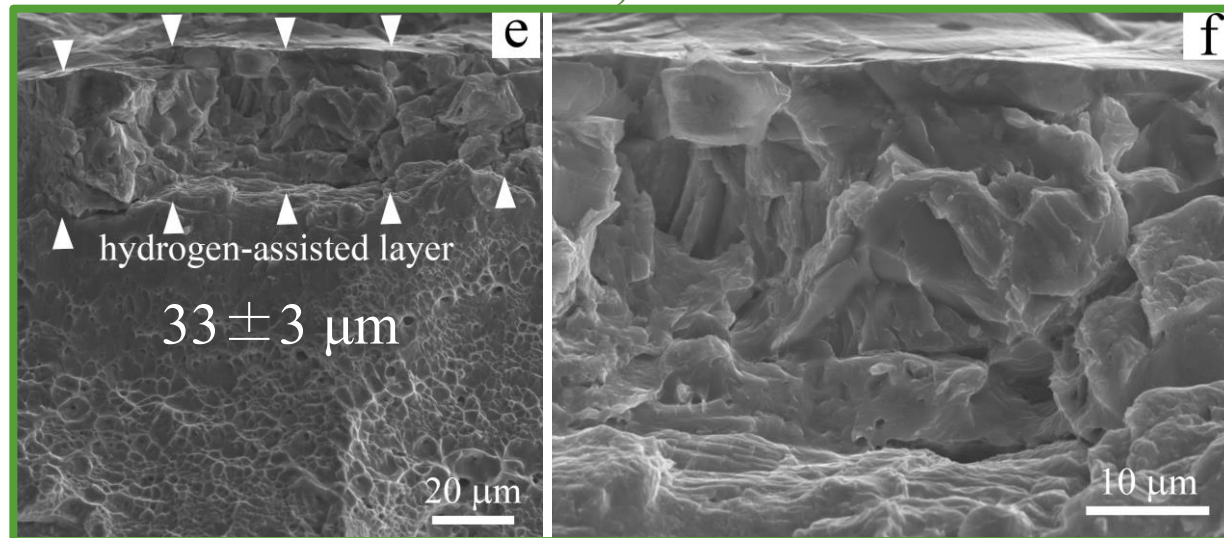
1050°C, 0.5 h



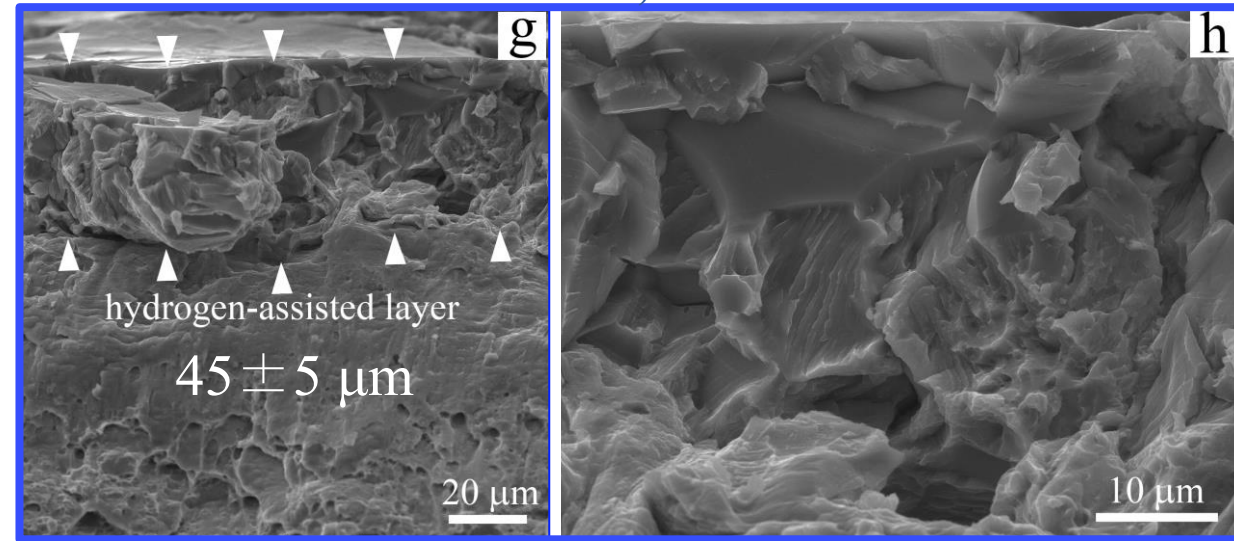
1100°C, 0.5 h



1150°C, 0.5 h



1200°C, 0.5 h



SUMMARY

- The decrease of the grain size of δ -ferrite and austenite and the volume fraction of δ -ferrite in HNS contributes to the decrease of the diffusion of hydrogen atoms deeply into the samples and causes the decrease of the effects of hydrogen embrittlement.
- The decrease of the density of interphase and grain boundaries in HNS specimens leads to the change in the fracture mechanism of the hydrogen-assisted layer – it promotes the contribution of intergranular fracture.

THANK YOU FOR YOUR ATTENTION!